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Constructing a filler network for thermal conductivity enhancement in epoxy composites via reaction-induced phase separation

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Abstract

Diglycidyl ethers of bisphenol-A (DGEBA)/methyl tetrahydrophthalic anhydride/polyethersulphone (PES) blends are prepared as matrix resins for thermally conductive composites using graphite nanoplatelets (GNPs) as the conductive component. The epoxy/PES blends form a network structure via reaction-induced phase separation (RIPS) during the curing process, and the GNPs are selectively localized in the PES phase and at the interface leading to a three-dimensional continuous filler network. With this unique structure, the thermal conductivity of the epoxy/PES/10 wt% GNPs composite is increased to $0.709 \text{ W m}^{-1} \text{ K}^{-1}$, which is nearly 3.5 times that of the pure epoxy or a 52% increase compared to the epoxy/GNP composite without PES. In addition, it is found that the impact strength of the composite relative to the unfilled

material is also improved.

Keyword: A. Polymer-matrix composites (PMCs); B. Thermal properties; E. Cure

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1. Introduction

As the growth in development and use of electronic and electrical equipment continues unabated so also does the requirement for materials that can deal with the heat generated by such equipment. Without highly efficient thermal management, this heat generation can significantly lower lifetime and reliability of electrical components [1, 2]. Since the majority of new electronic/electrical products are today made from a polymer based material which is intrinsically thermally insulating, there is an urgent need to develop new polymeric materials that are thermally conductive [3-5].

A variety of fillers such as carbon nanotubes [6, 7], boron nitride [8-11], graphene nanoplatelets [12, 13], silicon carbide [14-16] and hybrid fillers [17-19] have been used to enhance the thermal conductivity of polymers because of their high thermal conductivity and large aspect ratio [20-23]. Various factors affect the thermal conductivity enhancement in the filled composites, such as the interfacial thermal

resistance [24-27], the size [28, 29] and type [18, 30, 31] of fillers and the distribution of fillers [12, 32, 33].

To achieve a high thermal conductivity in a composite it is essential to achieve a network of the conductive particles in the polymer matrix [34, 35]. Building such networks in a polymer composite has been the subject of significant research effort in recent years. One method is to design a segregated structure [8, 10, 12, 33-38] including three steps: (1) fabrication of micron-sized polymer particles; (2) coating of conductive fillers onto the surface of the polymer particles; and (3) compression molding of the filler coated polymer particles. This is a relatively straightforward method but the compression moulding process itself is not commercially significant and therefore of limited interest. Another approach is to construct a freestanding filler framework as the heat transfer network, such as a graphene aerogel [39-41], BNNS aerogel [42, 43] or complex aerogel [9, 44-46], and then encasing the network in a thermosetting matrix such as epoxy. Jiang et al. [9] prepared a cellulose nanofiber supported boron nitride aerogel via sol-gel and freeze-drying, followed by casting with epoxy. The composites exhibit thermal conductivity enhancement of about 1400% at a low BNNS loading of 9.6 vol%. However, this method normally needs multiple processing steps, and it is time-consuming and difficult for large-scale fabrication.

Another approach is the selective distribution of fillers in an immiscible polymer blend with a co-continuous structure [33, 47-51], a strategy that has also been applied in

the design of electrically conductive composites [52-55]. For example, it has been found that silicon carbide will aggregate in a single polymer phase in an immiscible PS/PVDF blend to form an efficient thermally conductive network [33]. Due to the simplicity of melt blending, this method has good commercial potential (to the best of our knowledge this approach is used mainly with thermoplastic/thermoplastic systems and is rarely reported for thermosetting systems). While the selective distribution of fillers at the interface can result in a continuous network of fillers at a low filler loading [32], this is not easy to achieve experimentally. One method however that offers some potential is that of reaction-induced phase separation (RIPS) of thermosetting/thermoplastic resin composite systems [56-59]. These blends can form sea-island structures, co-continuous phase structures or phase inversion structures depending on the content of thermoplastic thus offering a potential strategy for better control of the network formation in a composite. This approach is adopted in the current work whereby a polyethersulphone (PES) modified-epoxy system is selected as the matrix and graphite nanoplatelets (GNPs) selected as the thermally conductive filler to produce thermally conductive composites. The effect of GNP content on the thermal conductivity and mechanical properties of the composites is investigated. Compared to the co-continuous structures obtained in previous work, the network-density of the phase inversion structure in this paper is improved. In addition, the straightforward preparation method and ability to easily tune the thermal conductivity of the composites has good potential for scale up to

more commercial applications.

2. Experimental

2.1 Materials

Graphite nanoplatelets (GNPs) (diameter: 5~40 μm , thickness: <100 nm, density: 0.25~0.3 g/cm^3) were supplied by Changzhou MoZhiCui technology Co. Ltd., China. The epoxy resin was a low molar mass liquid diglycidyl ether of bisphenol A (E51) provided by Nantong Xingchen Synthetic Material Co. Ltd, China. Polyethersulfone (PES, number-average molecular weight: $M_n = 6.7 \times 10^4$ and an intrinsic viscosity of 0.36 dL/g) was supplied by Jilin University, China. The curing agent was methyl tetrahydrophthalic anhydride (MTHPA), purchased from Zhejiang Alpha Chemical Technology Co. Ltd. 2-ethyl-4-methylimidazole (Sinopharm Group Chemical Reagent Co. Ltd., China) was used as an accelerator.

2.2 Composite Preparation

The epoxy/PES/GNPs composites were made using the following procedure. Firstly, the PES powder was mixed with the liquid curing agent MTHPA at room temperature. The mixture was heated in an oil bath at 110 $^{\circ}\text{C}$ for 2 h to dissolve the PES in the liquid MTHPA. After the mixture was cooled to 90 $^{\circ}\text{C}$, the required amount of epoxy (epoxy: MTHPA = 5 : 4, by weight ratio) was added to the mixture under continuous stirring for 30 min. Then, different contents of GNPs (1 wt%, 3 wt%, 5 wt%, 7 wt%, 10 wt% and

15 wt% of epoxy/PES blend) were added with mechanical stirring for 30 min, and the mixture was degassed. The compositions were cured at 145 °C for 4 h. Fig. 1 shows the processing steps used to fabricate the composites. Epoxy/2-ethyl-4-methylimidazole/GNPs composites without PES were also prepared as a reference material.

2.3 Characterization

2.3.1 Contact angle measurements

The surface tension of all the components was measured using contact angle measurements. Before the measurement, films of PES and GNPs were prepared by hot-pressing [60] and the uncured epoxy was coated on a glass slide [61]. Contact angle was measured at 25 °C with a drop shape analysis system (DSA100, KRUSS). Measurement of a given contact angle was carried out at least 5 times. Double distilled water (H₂O) and methylene iodide (CH₂I₂) were used as probe liquids. The dispersive and polar components of the surface tension are 22.5 and 50.5 dyn cm⁻¹ for water and 48.5 and 2.3 dyn cm⁻¹ for methylene iodide, respectively [62].

2.3.2 Thermal conductivity measurements

The thermal conductivity was measured using a Hot Disk thermal analyzer (TPS-2500), and based upon the transient plane source (TPS) method [63]. The dimension of the samples was 30×30×8 mm with the sensor placed between two similar slabs of materials. The sensor supplied a heat pulse of 0.08 W for 5 s to the sample and

the subsequent change in temperature was recorded. The thermal conductivity of the samples was obtained by fitting the data according to Gustavsson et al. [64]. The temperature of the composites was recorded using an infrared thermograph (FOTRIC 220).

2.3.3 Scanning electron microscopy (SEM), optical microscopy (OM) and transmission electron microscopy (TEM)

The microstructure of the cured epoxy blends and dispersibility of the GNPs filler were observed using a JSM-6510 scanning electron microscope (SEM, Jeol, Japan) and a metallographic microscope (Axio Observer A1m, Carl Zeiss Jena, Germany). The internal microstructure of the composites was characterized using transmission electron microscopy (TEM). The TEM measurements were performed using a Technai 12 transmission electron microscope (FEI) at an acceleration voltage of 120 kV. To prepare the SEM samples, the specimens were first fractured in liquid nitrogen and then sputter-coated with a thin layer of gold. SEM measurements were performed on a SEM (JSM-6510). To prepare the TEM samples (70 nm thickness), the composites were ultra-microtomed at room temperature using an ultramicrotome (Leica EM UC6). In order to observe the epoxy/PES blend structure, the material was sandwiched between two glass slides and cured at 145 °C for 2 h and observed in transmission mode. For the epoxy/PES/GNP composite structure, the specimen was polished with emery paper and observed in reflection mode.

2.3.4 Impact strength measurement

Un-notched Izod impact testing was carried out on an Izod impact test machine (UJ-4, Chengde Machine Factory, China) according to ASTM D4812–2004.

3. Results and discussion

3.1 Prediction for selective distribution of GNPs

For the distribution of fillers in immiscible polymer blends, many studies have demonstrated that the factors affecting distribution of fillers are complex [65-68] and it is difficult to give a completely accurate prediction of the distribution. However, the surface tension of each component in the blend is considered an important factor for prediction of distribution. Based on thermodynamics, the wetting coefficient (ω_a) suggested by Sumita et al. [69] is widely and relatively successfully used to forecast distribution [32, 49, 60]. Wetting coefficient (ω_a) can be calculated according to equation (1):

$$\omega_a = \frac{\gamma_{\text{GNPs-B}} - \gamma_{\text{GNPs-A}}}{\gamma_{\text{A-B}}} \quad (1)$$

where $\gamma_{\text{GNPs-B}}$ is the interfacial tension between the GNPs and polymer B, $\gamma_{\text{GNPs-A}}$ is the interfacial tension between GNPs and polymer A, and $\gamma_{\text{A-B}}$ is the interfacial tension between polymers A and B. If $\omega_a < -1$, GNPs will be located in polymer B. If $-1 < \omega_a < 1$, GNPs will be located at the interface of the blend. If $\omega_a > 1$, GNPs will be preferentially

located in polymer A.

The interfacial tension between two components, γ_{A-B} , can be calculated using the harmonic mean equation and the geometric mean equation [70].

The harmonic mean equation:

$$\gamma_{A-B} = \gamma_A + \gamma_B - 4 \left(\frac{\gamma_A^d \gamma_B^d}{\gamma_A^d + \gamma_B^d} + \frac{\gamma_A^p \gamma_B^p}{\gamma_A^p + \gamma_B^p} \right) \quad (2)$$

and the geometric mean equation:

$$\gamma_{A-B} = \gamma_A + \gamma_B - 2 \left(\sqrt{\gamma_A^d \gamma_B^d} + \sqrt{\gamma_A^p \gamma_B^p} \right) \quad (3)$$

where γ_i is the surface tension of component i. γ_i^d is the dispersive portion of the surface tension of component i, and γ_i^p is the polar portion of the surface tension of component i.

Surface tension, γ_i , is the sum of γ_i^d and γ_i^p , and can be calculated from the contact angle θ . The relationship between θ and γ_i is described using Owens-Wendt [71].

$$\gamma_L (1 + \cos \theta) = 2 \sqrt{\gamma_s^d \gamma_L^d} + 2 \sqrt{\gamma_s^p \gamma_L^p} \quad (4)$$

where γ_L is the surface tension of the liquid and γ_L^d and γ_L^p are the dispersive and polar portions, respectively, of the liquid's surface tension.

The contact angles of H₂O on the surfaces of PES, epoxy and GNPs were 73.0°, 58.5°, and 71.7°, respectively. The CH₂I₂ contact angles on the surfaces of PES, epoxy and GNPs were 50.5°, 22.7° and 28.8°, respectively. The surface energies were calculated using Equation (4) and are shown in Table 1). The interfacial tensions

between each of the components were calculated according to Equation (2) and (3), and are shown in Table 2. Finally, wetting coefficient data for the epoxy/PES blends filled with GNPs were calculated according to Equation (1), and are shown in Table 3.

The value of wetting coefficient data lies between $-1 \sim 1$, hence it is predicted that the GNPs will tend to be selectively located at the interface of the PES phase and the epoxy phase.

3.2 Microstructure of the epoxy/PES blends

The morphologies of cured composites at various epoxy/PES weight ratios (epoxy/PES = 10w/1w, 10w/2w, 10w/3w) were characterized using OM (Fig. 2). At 10 wt% of epoxy, the PES formed a large number of small domains (Fig. 2a); at 20 wt%, a co-continuous phase structure was observed (Fig. 2b); and at 30 wt%, phase inversion occurred (i.e., epoxy forms small phase domains throughout the PES matrix) (Fig. 2c).

Fig. 3 shows the phase inversion structure of the fractured surface of epoxy/PES (epoxy/PES = 10w/3w). The phase components were analyzed using SEM and energy dispersive spectrometry [72]. The results reveal that the network phase (area 2) contains a greater amount of sulfur compared to the isolated spherical domain phase (area 1), meaning that the network phase is the PES phase, and the isolated spherical domain phase is the epoxy phase. Among the epoxy/PES compositions, epoxy/PES (epoxy/PES = 10w/3w) was chosen as a suitable matrix composition, because a phase inversion structure was expected to be a favorable template for distributing GNPs to form an

effective network.

3.3 Microstructures of epoxy/PES/GNP composites

Fig. 4 shows the cross-section of the epoxy/PES/GNP and epoxy/GNP composites with various filler content. In the epoxy/PES/GNPs composites (Fig. 4A~D), it can be seen that PES formed a continuous phase in the blends and GNPs were observed in it. In other words, the GNPs were selectively distributed at the interface of the blends or in the PES phase. Additionally, the cross-section images demonstrate that GNPs gradually contact with each other to form a filler pathway with increasing GNP content. When GNP content increased to 10 wt%, the GNPs tended to connect together to construct a filler network. However, a further increase in GNP content (15 wt%) led to significant changes in the morphology of the composite, and only a few epoxy domains are clearly observed in Fig. 4D. This occurs because when the GNP content reaches 15 wt%, the difference in matrix viscosity increases rapidly and the compatibility of the matrix changes, which in turn leads to an incomplete phase inversion structure, as shown in Fig. 4D and Fig. 5D. This means that a 3D interconnected template is not formed and thus a 3D interconnected filler network is not formed [52, 73]. For comparison, the distribution of GNPs in the epoxy composites without PES is random, as shown in Fig. 4a~d.

Due to the reflective characteristic of GNPs, the distribution of GNPs can also be

clearly observed by OM as shown in Fig. 5. In Fig. 5A and 5B, the arrows indicate the locations of GNPs (GNPs are observed as white spots under xenon lamp irradiation), the filler network structure has not yet been built. When the filler content reaches 10 wt%, the filler network is formed. These results are consistent with the SEM observations.

Both SEM and OM images provide a powerful and direct proof of GNP network formation throughout the entire matrix, but TEM is required to observe the detailed location of GNPs.

The selective distribution of GNPs in the composites was visualized using TEM (Fig. 6). The dark gray domain is the PES phase, whereas the light gray domain is the epoxy phase. GNPs (shown by arrows) are located at the interface, and also in the PES phase near the interface which may have resulted from a smaller interfacial tension between the PES and GNPs. This observation is generally consistent with the prediction based on wetting coefficient.

3.4 Thermal conductivity of epoxy/PES/GNPs composites

Fig. 7 shows the thermal conductivities of epoxy/GNPs and epoxy/PES/GNPs (epoxy/PES = 10w/3w) composites with different GNPs content.

The thermal conductivity of epoxy/PES/GNPs composites and epoxy/GNPs composites are relatively close when the GNPs content is small (1~7 wt%). However, significant enhancement was observed in the thermal conductivity of epoxy/PES/GNPs

composites as GNPs content increased to 10 wt% comparing with epoxy/GNPs composites at the same filler loading. This demonstrates that 10 wt% GNPs content may be a critical level for these epoxy composites. At small GNPs content, there are insufficient GNPs to form a percolated, thermally conductive pathway. With further increases in GNPs content, thermal conductivity in epoxy/PES/GNPs composites increases remarkably. This is attributed to the formation of a three-dimensional filler network via RIPS. Therefore, improved thermal conductivity of epoxy composites can be achieved efficiently by the formation of filler network via RIPS, i.e. the thermal transfer efficiency per unit mass of filler is increased by this strategy.

In order to demonstrate the thermal performance of epoxy/PES/10 wt% GNPs composites, the surface temperature variations of the composites with time during heating were recorded using an infrared thermograph. All the samples were placed on a hot stage at 80 °C. The epoxy/PES/10 wt% GNPs composite has a much better thermal response due to its higher thermal conductivity, and the surface temperature of epoxy/PES/10 wt% GNPs composite continuously increases with time, at a higher rate, as shown in Fig. 8. These results illustrate that epoxy/PES/10 wt% GNPs composite has enhanced thermal conductivity.

3.5 Impact strength of epoxy/PES/GNPs composites

The impact strength of epoxy/PES/GNPs composites is shown in Table 4. It can be seen that the impact strength of pure epoxy and epoxy/PES without GNPs have little

differences, but the impact strength of epoxy composites with 1~10 wt% GNPs increases by 10~30% relative to pure epoxy. The GNPs which are located at the interface and in PES phase near the interface, may have enhanced the binding force of the interface and the toughness of the PES phase [74]. However, when the GNPs content reaches 15 wt%, the impact strength decreases again. This may be due to aggregates of GNPs acting as stress concentrators [25].

4. Conclusions

Using RIPS, an epoxy/PES blend can form a phase inverted structure. This phase inverted structure functions as a template for GNPs to form a three-dimensional connected network structure. The self-assembled structure of GNPs within the PES phase leads to a composite with a high thermal conductivity at a relatively low GNPs loading. This concept is illustrated in Fig. 9. Impact strength tests indicate that mechanical properties of these composites are not compromised.

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Figures caption:

Fig. 1 Schematic showing the preparation of epoxy/PES/GNPs composites.

Fig. 2 OM images of epoxy/PES composites with various weight ratios: (a) 10w/1w; (b) 10w/2w; (c) 10w/3w.

Fig. 3 SEM micrographs of phase inversion structure. The elemental content of areas in the micrographs was analyzed by energy dispersive spectrometer.

Fig. 4 SEM images of epoxy/PES/GNPs and epoxy/GNPs composites at different GNP contents. Epoxy/PES/GNPs: (A) 3 wt% GNPs; (B) 7 wt% GNPs ; (C) 10 wt% GNPs; (D) 15 wt% GNPs; epoxy/GNPs: (a) 3 wt% GNPs; (b) 7 wt% GNPs ; (c) 10 wt% GNPs; (d) 15 wt% GNPs.

Fig. 5 OM images of epoxy/PES/GNPs and epoxy/GNPs composites at different GNPs contents. Epoxy/PES/GNPs: (A) 3 wt% GNPs; (B) 7 wt% GNPs ; (C) 10 wt% GNPs; (D) 15 wt% GNPs; epoxy/GNPs: (a) 3 wt% GNPs; (b) 7 wt% GNPs ; (c) 10 wt% GNPs; (d) 15 wt% GNPs.

Fig. 6 TEM images of the GNP distribution in (a) the epoxy/PES/1 wt% GNPs composite and (b) the epoxy/PES/7 wt% GNPs composite.

Fig. 7 Thermal conductivities of epoxy/PES/GNPs and epoxy/GNPs composites as a function of GNP content.

Fig. 8 (a) IR images of (①) pure epoxy, (②) epoxy/10 wt% GNPs and (③) epoxy/PES/10 wt% GNPs with heating time; (b) surface temperature variation of samples with heating time

Fig. 9 Structure evolution of thermally conductive epoxy/PES/GNPs composites with RIPS

Table 1 The surface energy data of components.

Table 2 Interfacial tensions γ_{A-B} between different components calculated using the harmonic and geometric mean equations.

Table 3 Wetting coefficient as calculated using the harmonic and geometric mean equation.

Table 4 The impact strength of pure epoxy and epoxy composites

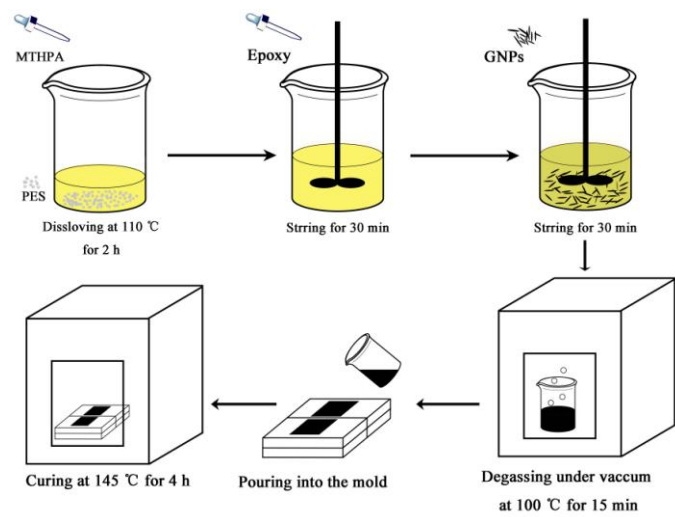


Fig. 1

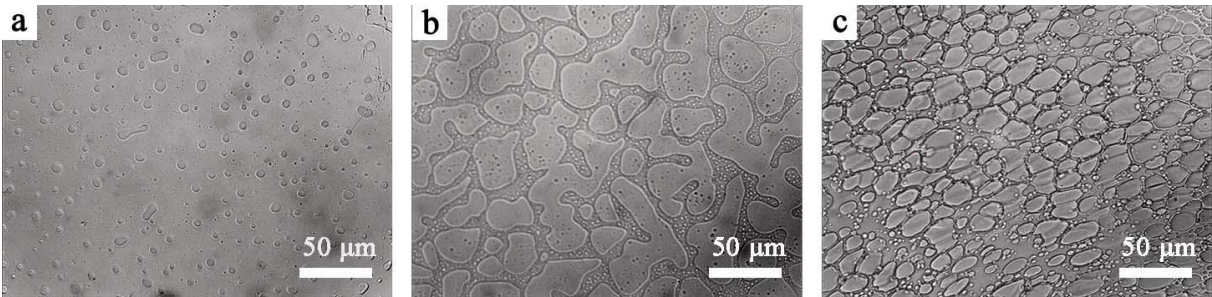


Fig. 2

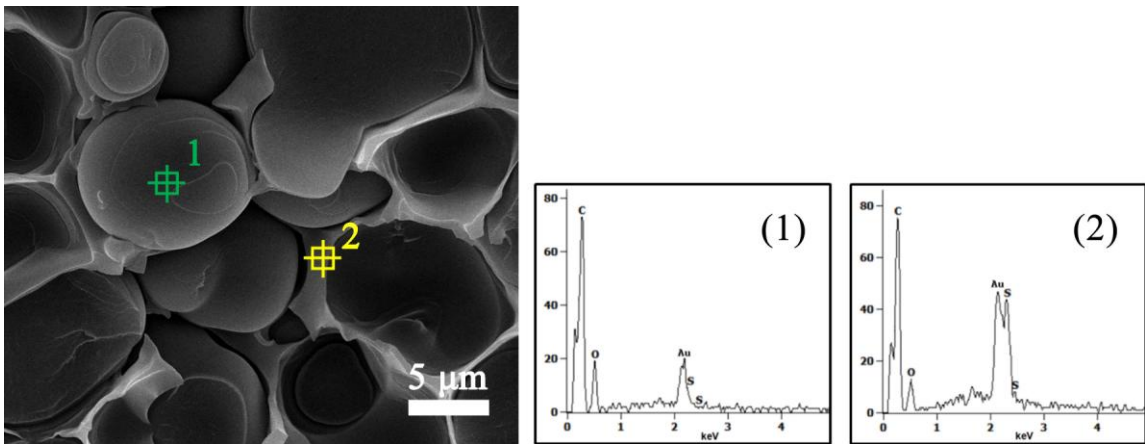


Fig. 3

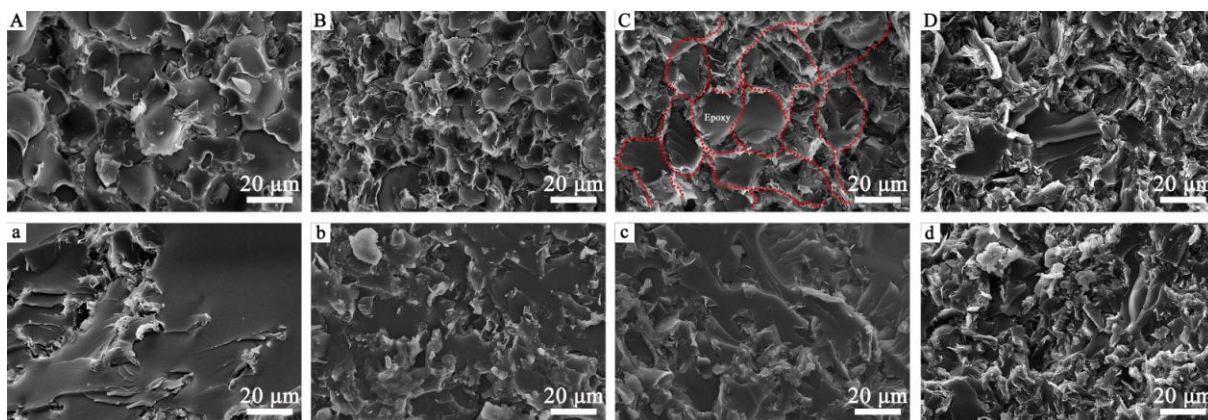


Fig. 4

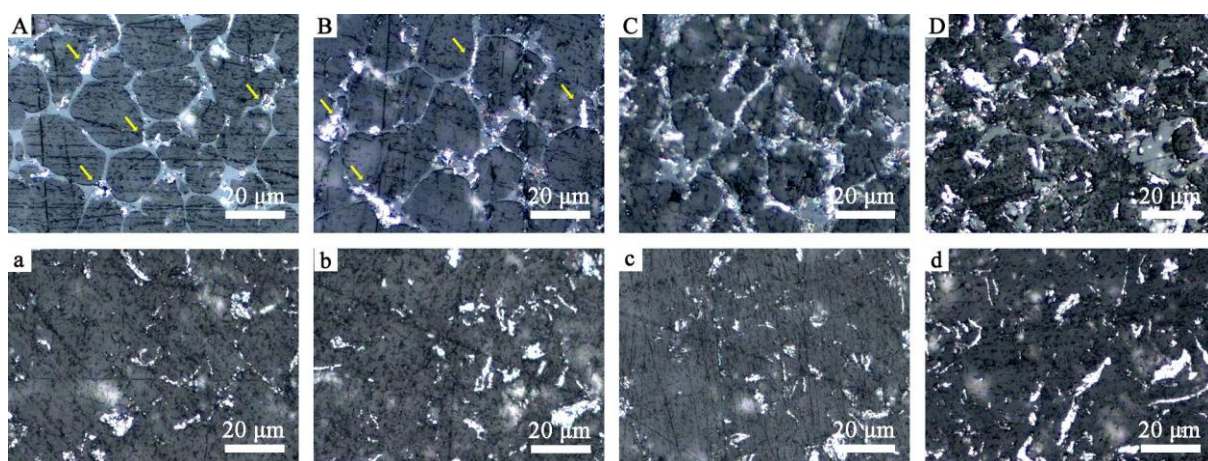


Fig. 5

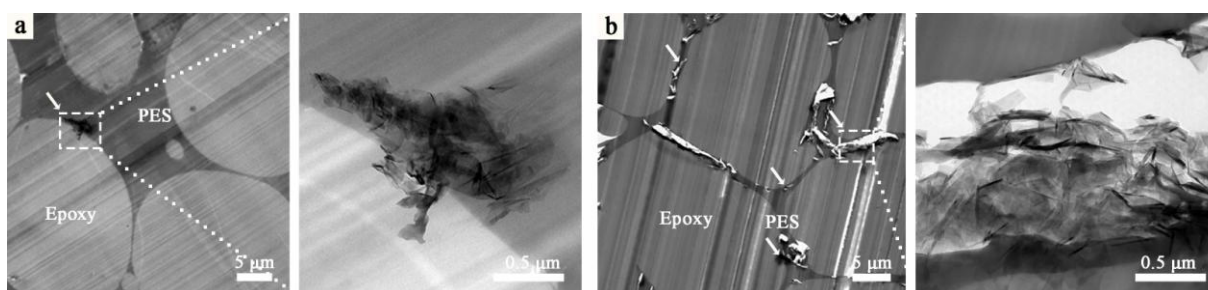


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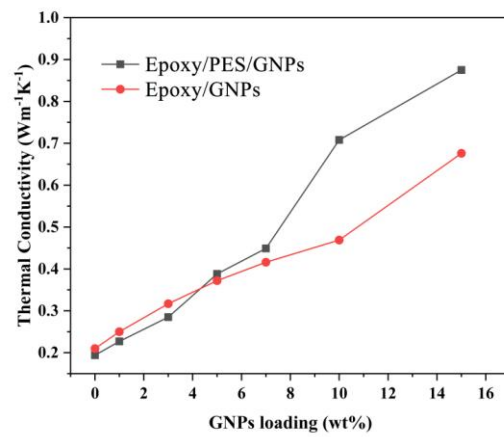


Fig. 7

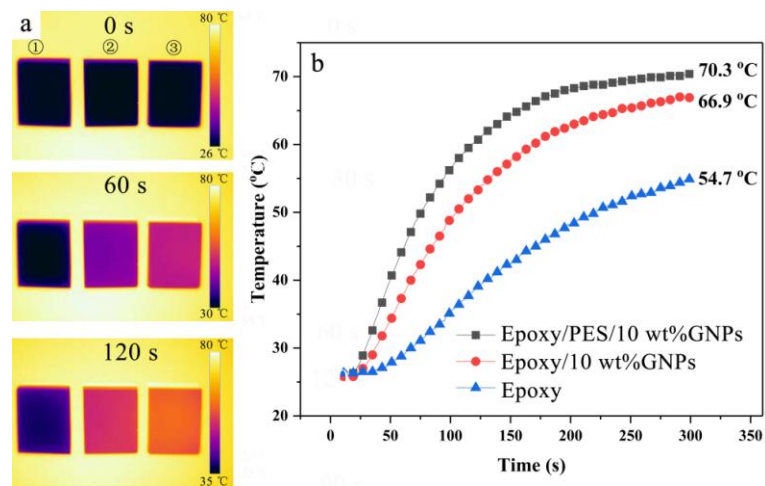


Fig. 8

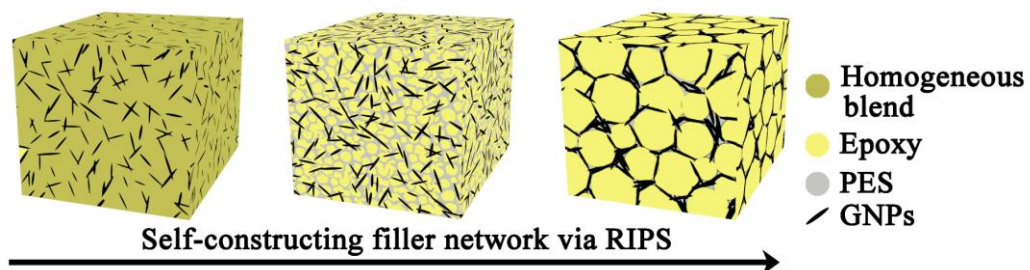


Fig. 9

Components	γ^d (mN m ⁻¹)	γ^p (mN m ⁻¹)	γ (mN m ⁻¹)
PES	27.9	9.8	37.7
Epoxy	38.5	13.7	52.2
GNPs	39.5	6.6	46.1

Table 1

Component couple	γ_{A-B} (mN m ⁻¹)	
	Based on the harmonic mean	Based on the geometric mean
	equation	equation
PES-GNPs	2.62	1.48
Epoxy-GNPs	2.50	1.29
PES-Epoxy	2.64	1.48

Table 2

Composite	ω_a calculated from the	ω_a calculated from the
	harmonic mean equation	geometric mean equation
Epoxy/PES/GNPs	0.05	0.02

Table 3

Matrix	GNPs content (wt%)	Impact strength (kJ m ⁻²)
Pure Epoxy	0	3.66 ± 0.53
Epoxy/PES	0	3.49 ± 0.55
Epoxy/PES	1	4.77 ± 0.73
Epoxy/PES	3	4.18 ± 0.95
Epoxy/PES	5	4.65 ± 0.48
Epoxy/PES	7	4.06 ± 0.55
Epoxy/PES	10	4.48 ± 0.42
Epoxy/PES	15	3.70 ± 0.39

Table 4